

# Variation and Calibration Error in Electronic Imaging

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## Abstract

In acquiring digital images, electronic systems not only detect optical signals but also convert them into a digital form for further image processing and exchange. Practical systems can introduce error during color calibration, and when acquiring image scene information. For large populations, it is often assumed that the error can be modeled as a random variable having a zero mean. In the case of a single color instrument, camera or scanner, however, error due to deterioration of a physical standard, optical filter or detector will introduce a bias into the measurement or image data. This error is modified as the signals are transformed (processed) into their final form. An error-propagation method is shown to describe the influence of the data-processing path on the magnitude of bias error. This approach is related to the propagation of image noise, or variance. The analysis is applied in examples drawn from color-measurement and digital image processing.

## Introduction

When making color measurements, we can think of instrument uncertainty as introducing an error into the (color) signal of interest. The same can be said of the acquisition of a digital image where pixel-to-pixel noise and color calibration errors can occur. We often assume that the error can be modeled as a random variable having a zero mean. For a single color instrument, however, a calibration error can introduce a consistent bias.

Color-measurement signals and digital images are usually transformed between several common color spaces. Therefore, an analysis of the way signal transformations influence the magnitude of color-signal error is useful when comparing performance with system tolerances.<sup>1,2</sup> These results can then be used to set limits for both instruments and physical standards.

One tool for the evaluation of error or variation in signal processing is error-propagation analysis,<sup>3</sup> where specific signal processing steps can be described by their corresponding transformations of the error statistics. The most common use of this method is the propagation of the second-order statistics, variance and RMS error.

Livens<sup>4</sup> addressed the combination of stochastic instrument errors and signal quantization. He showed that the combined variance is found by adding the effective variance of each noise source, as for independent sources. Gonzalez, *et al.*, evaluated the practical limits to color accuracy in terms of the color-difference metric,  $\Delta E_{94}^*$ . They compared results with and without color management, and pointed out requirements for ICC device profiles.

In this paper, we address the propagation of first-order statistical error, bias. This can be applied to a consistent error component due to, e.g., instrument drift, deterioration of a physical standard, or signal quantization.

## Bias Error

If an observed signal is subject to error, it can be expressed as the sum of true value and bias,

$$\hat{p} = p + b_p,$$

where  $\hat{p}$  is the observed value,  $p$  the true value, and  $b_p$  the bias error. For many measurements or digital images, both the true and bias values vary, so we can define the bias using statistical expectations

$$b_p = E[\hat{p}] - \mu_p. \quad (1)$$

where  $E$  is the expected value and  $\mu_p$  is the true (unbiased) mean.

A matrix-vector notation is usually adopted for systems with related sets of (color) signals. This is used in the Appendix, where the transformation, or scaling, of the bias error due to signal transformations is approximated using a derivative matrix in Eq. (a7).

## Matrix

The propagation of bias error for a simple matrix transformation of a set of color signals can be understood as a special case of Eq. (a6). For example,

$$\mathbf{q} = \mathbf{M}\mathbf{p}. \quad (2)$$

Since each element of the matrix,  $\mathbf{M}$ , is a constant, the elements of the first derivative matrix,  $\mathbf{J}_M$ , are simply the matrix coefficients. The resulting bias in  $\mathbf{q}$  is,

$$\mathbf{b}_q \equiv \mathbf{M}\mathbf{b}_p \quad (3)$$

**XYZ to CIELAB**

Bias error propagation for a common colorimetric transformation, from tristimulus values (X,Y,Z) to CIELAB coordinates (L\*, a\*, b\*) can be also be modeled. Here we assume that the bias in the measured tristimulus values is that evident after the division by those of the white reference, (X<sub>n</sub>, Y<sub>n</sub>, Z<sub>n</sub>). For values of X/X<sub>n</sub>, Y/Y<sub>n</sub>, Z/Z<sub>n</sub> > 0.00886 the derivative matrix is

$$\mathbf{J} = \begin{bmatrix} 0 & 116 & 0 \\ 500 & 3\mu_Y^{2/3} & 0 \\ 3\mu_X^{2/3} & -500 & 0 \\ 0 & 3\mu_Y^{2/3} & 200 \\ 0 & 3\mu_Y^{2/3} & -3\mu_Z^{2/3} \end{bmatrix} \quad (4)$$

The bias propagation is given by Eq. (a6),

$$\mathbf{b}_{L^*a^*b^*} \equiv \mathbf{J} \mathbf{b}_{XYZ} \quad (5)$$

McDowell<sup>6</sup> gave several 'rules of thumb' for the propagation of reflectance factor measurement error to CIELAB. He investigated the relationship between spectral reflectance error and CIELAB ΔE<sub>ab</sub><sup>\*</sup> using the 928 color patches of the ANSI IT8.7/3 CMYK output characterization target.

He found that a neutral 2% change in the measured X, Y, Z values (from reflectance factor measurements) resulted in an average ΔE<sub>ab</sub><sup>\*</sup> of 0.5 and a maximum of 0.9. If, however, the error was in the Z value, due to yellowing of the white reference, the average ΔE<sub>ab</sub><sup>\*</sup> was 0.9. Similarly, leaving the Y and Z values unchanged and changing the X value by 2% resulted in an average ΔE<sub>ab</sub><sup>\*</sup> = 1.8.

If we interpret these instrument errors as bias introduced into the X, Y, Z values, the above error-propagation analysis can be compared with McDowell's computed results. This was done and the results do predict the actual measurement results. Table 1 summarizes the comparison. Figure 1 shows the ΔE<sub>ab</sub><sup>\*</sup> that results from a 2% nonselective bias, plotted as an a\*-b\* surface for μ<sub>L\*</sub> = 50.

**CRT Gamma**

A common color encoding specification for the interchange of digital images is sRGB.<sup>7,8</sup> This was developed to facilitate viewing of images on computer CRTs, and so includes the color characteristics of a reference monitor. This reference monitor is characterized by the monitor phosphor tristimulus values, and (mean) signal transfer function. The transfer function is modeled by an equation for output luminance.<sup>9</sup> For an input signal, d, [0-1] the resulting CRT luminance factor is

$$I = (k_1 d + k_2)^\gamma, \quad (6)$$

where k<sub>1</sub> and k<sub>2</sub> are the system gain and offset and γ is the CRT gamma. In general, the gain and offset values are under the control of the user, by way of the contrast and brightness controls. The gamma value is primarily set by the CRT design. Since most CRT color evaluations require estimation of the effective gamma, it is useful to understand the sensitivity of the above luminance model to variations in the gamma value. If a monitor deviates from expected performance by a bias in the gamma value, the bias propagation is given by Eq. (a4)

$$b_I = (d^{\mu_\gamma} \log_e d) b_\gamma, \quad (7)$$

where k<sub>1</sub> and k<sub>2</sub> have been set to 1 and 0. For a true value of μ<sub>γ</sub> = 2.2 and bias, b<sub>γ</sub> = 0.15, Fig. 2 shows the CRT transfer curves. The luminance factor bias that would result from this gamma error was then computed directly and via Eq. (7), with the results plotted in Fig. 3. The overestimation of the negative bias is due to the series approximation of Eqs. (a4) and (a6).

**Table 1. Comparison of bias analysis, via Eq. (4) and McDowell results (in italic), for the IT8 data set.**

	% bias			ΔE <sub>ab</sub> <sup>*</sup>	
	X	Y	Z	average	max.
Nonselective	-2	-2	-2	0.46 <i>0.5</i>	0.87 <i>0.9</i>
Low X	-2	0	0	1.80 <i>1.8</i>	3.01 <i>3.0</i>
Low Y	0	-2	0	1.96	3.32
Yellowing		0	-2	0.68 <i>0.7</i>	1.18 <i>1.2</i>

L\* = 50

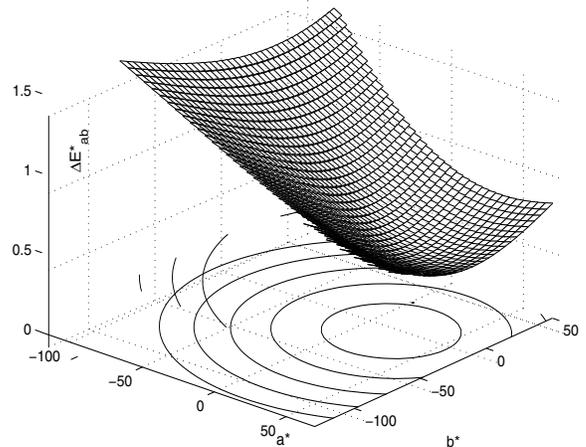


Figure 1. ΔE<sub>ab</sub><sup>\*</sup> for 2% bias in X, Y, Z for μ<sub>L\*</sub> = 50.

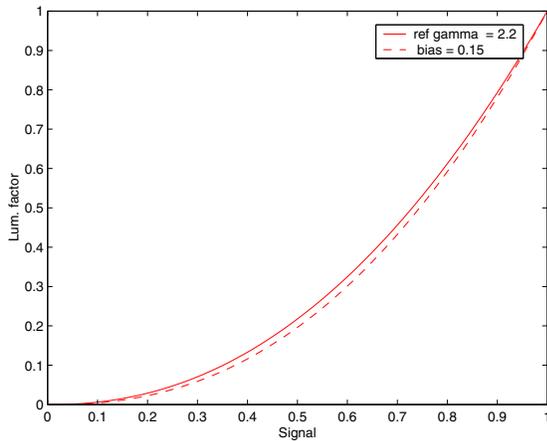


Figure 2. CRT characteristics:  $\gamma = 2.2$  and  $b_\gamma = 0.15$

The derivative matrix of Eq. (4) was then used to propagate the luminance factor error to CIELAB. The resulting bias in  $L^*$  is plotted in Fig. 4. We again observe good agreement between bias error-propagation and direct calculation.

## Conclusions

The analysis of the propagation of bias errors during signal processing can be used in conjunction with direct error computation. In all cases described, the error propagation method gave similar results to those computed directly. The method, therefore, can be expected to provide predictions of color measurement and calibration performance for a wide range of practical transformations. In many cases, the error transformations can be inverted, facilitating their application to component tolerancing and subsystem specification.

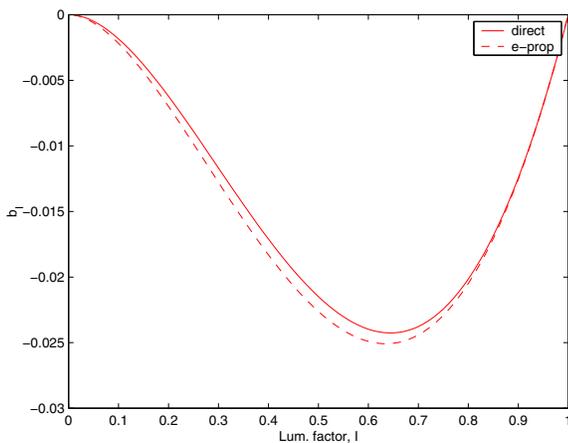


Figure 3. Luminance factor [0-1] bias for  $b_\gamma = 0.15$ . The solid line is the point-by-point difference, dashed is from bias equation.

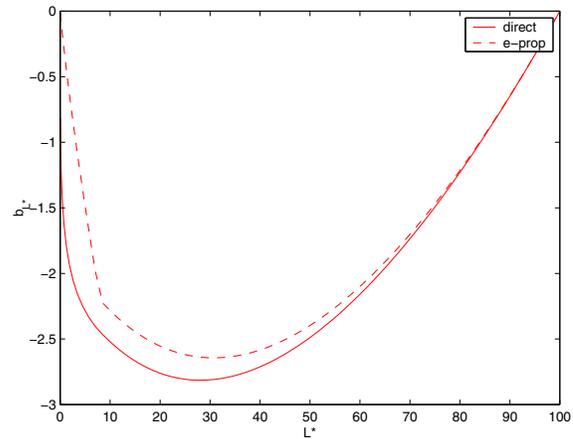


Figure 4. Bias in  $L^*$  due to  $b_\gamma = 0.15$ , (in  $L^*$  units [0-100]). The solid line is the point-by-point difference, dashed is from bias equations.

## Acknowledgements

Many thanks to David McDowell for sharing his experience and data, and Gustav Braun for his suggestions.

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### Appendix I: Bias of a Function of a Biased Random Variable

We are given the function  $f(x)$  of the random variable,  $x$ , which is corrupted with a bias error. If  $\hat{x}$  is the biased random variable, its expected value can be written as

$$E[\hat{x}] = b_x + \mu_x \tag{a1}$$

where  $b_x$  is the bias and  $\mu_x$  is the true (expected) value. We define the bias of  $f(x)$  as

$$b_f = E[f(\hat{x})] - f(\mu_x) \tag{a2}$$

If we expand  $f$  about  $\mu_x$  in a Taylor series and take expectations

$$E[f(\hat{x})] \cong f(\mu_x) + f'(\mu_x)b_x + 0.5f''(\mu_x)\sigma_x^2, \tag{a3}$$

where

$$f'(\mu_x) = \left. \frac{\partial f}{\partial x} \right|_{x=\mu_x} \quad \text{and} \quad f''(\mu_x) = \left. \frac{\partial^2 f}{\partial^2 x} \right|_{x=\mu_x}.$$

Substituting Eq. (a3) into Eq. (a2), the bias error in  $f(x)$  can be approximated by

$$b_f \cong f' b_x + 0.5 f'' \sigma_x^2.$$

The RHS shows the two components of the bias in  $f$ . The first is due to the bias in  $\hat{x}$  and the second due to its variation. Here we will only consider the first source, bias, since it will usually dominate, so

$$b_f \cong f' b_x. \tag{a4}$$

Similar expressions can be developed for multivariate transformations. Let  $\mathbf{x}$  and  $\mathbf{y}$  be vectors, related by  $\mathbf{f}$

$$\mathbf{y} = \mathbf{f}(\mathbf{x}), \tag{a5}$$

where

$$\mathbf{x} = [x_1, x_2, \dots, x_n]^T, \quad \mathbf{y} = [y_1, y_2, \dots, y_m]^T,$$

$$\mathbf{f}(\mathbf{x}) = \begin{bmatrix} f_1(x_1, x_2, \dots, x_n) \\ f_2(x_1, x_2, \dots, x_n) \\ \vdots \\ f_m(x_1, x_2, \dots, x_n) \end{bmatrix}$$

and for color image processing,  $m = n = 3$ . If the bias in each component signal of  $\mathbf{x}$  is written as a vector

$$\mathbf{b}_x = [b_{x_1}, b_{x_2}, \dots, b_{x_n}]^T,$$

the output bias vector, is

$$\mathbf{b}_y \cong \mathbf{J}_f \mathbf{b}_x, \tag{a6}$$

where

$$\mathbf{J}_f = \begin{bmatrix} \frac{\partial y_1}{\partial x_1} & \frac{\partial y_1}{\partial x_2} & \dots & \frac{\partial y_1}{\partial x_n} \\ \frac{\partial y_2}{\partial x_1} & \ddots & & \\ \vdots & & \ddots & \\ \frac{\partial y_m}{\partial x_1} & & & \frac{\partial y_m}{\partial x_n} \end{bmatrix}, \tag{a7}$$

and each element of  $\mathbf{J}_f$  is evaluated at  $(\mu_{x_1}, \mu_{x_2}, \dots, \mu_{x_n})$ .

### Biography

Peter Burns studied Electrical and Computer Engineering at Clarkson University, receiving his BS and MS degrees. In 1997, he completed his Ph.D. in Imaging Science at Rochester Institute of Technology. After working for Xerox, he joined Eastman Kodak's Imaging Research and Development organization. A frequent contributor to imaging conferences, his technical interests include; system evaluation, simulation, and the statistical analysis of error in digital and hybrid systems. peter.burns@kodak.com